An Improved Simplified Heat Stress Management Approach for the Non-Technical User

Dr Ross Di Corleto

Monitor Consulting Services



OSHA issues citations re Heat Stress

- In 2016 and 2017, OSHA issued five citations to the United States Postal Service (USPS) alleging Heat Stress violations in:
 - San Antonia and Houston, Texas;
 - Des Moines, Iowa;
 - Charleston, West Virginia; and
 - Benton, Arkansas.
- OSHA introduced the National Weather Service (NWS) heat index chart into the trial record and pointed to it as evidence.



National Weather Service Heat Index Chart

| 1 | NWS | He | at Ir | ndex | | | Τe | empe | rature | e (°F) | 1 | | | | | | |
|--------|-----|---------------|-----------------------|---------------------|-------------------|--------|------------|-------------------|--------------------|----------------------|---------------------|--------------------------|----------------------|---------------|-------------------------|------------|--|
| 1 | | 80 | 82 | 84 | 86 | 88 | 90 | 92 | 94 | 96 | 98 | 100 | 102 | 104 | 106 | 108 | 110 |
| | 40 | 80 | 81 | 83 | 85 | 88 | 91 | 94 | 97 | 101 | 105 | 109 | 114 | 119 | 124 | 130 | 136 |
| | 45 | 80 | 82 | 84 | 87 | 89 | 93 | 96 | 100 | 104 | 109 | 114 | 119 | 124 | 130 | 137 | |
| (%) | 50 | 81 | 83 | 85 | 88 | 91 | 95 | 99 | 103 | 108 | 113 | 118 | 124 | 131 | 137 | | |
| ž | 55 | 81 | 84 | 86 | 89 | 93 | 97 | 101 | 106 | 112 | 117 | 124 | 130 | 137 | | | |
| idi | 60 | 82 | 84 | 88 | 91 | 95 | 100 | 105 | 110 | 116 | 123 | 129 | 137 | | | | |
| Ę | 65 | 82 | 85 | 89 | 93 | 98 | 103 | 108 | 114 | 121 | 128 | 136 | | | | | |
| Ŧ | 70 | 83 | 86 | 90 | 95 | 100 | 105 | 112 | 119 | 126 | 134 | | | | | | |
| ive | 75 | 84 | 88 | 92 | 97 | 103 | 109 | 116 | 124 | 132 | | | | | | | |
| lat | 80 | 84 | 89 | 94 | 100 | 106 | 113 | 121 | 129 | | | | | | | | |
| Re | 85 | 85 | 90 | 96 | 102 | 110 | 117 | 126 | 135 | | | | | | | | |
| :95750 | 90 | 86 | 91 | 98 | 105 | 113 | 122 | 131 | | | | | | | | And No | AR |
| | 95 | 86 | 93 | 100 | 108 | 117 | 127 | | | | | | | | | | -) |
| | 100 | 87 | 95 | 103 | 112 | 121 | 132 | | | | | | | | | | and the second s |
| | | | Like Cautic | lihood on | l of He | at Dis | orders | s with Cautio | Prolor | nged E | Exposi | u re or Danger | Strenu | ious A | ctivity dreme | / Dange | er |
| | С | lassif Cau | icatio tion | n Hea 80°F | t Index - 90°F | Fatig | ue pos | sible w | Efi ith prole | fect on onged (| the boo exposu | dy re and/ | or phys | ical act | tivity | | |
| | | Extr Cau | eme tion | 9 1 | 0°F - 03°F | Ĥ | leat stro | oke, he rolong | at cram ed expo | ps, or l osure a | neat exl nd/or p | haustio hysical | n possi activity | ible wit / | h | | |
| | | Dar | iger | 10 |)3°F - 24°F | Heat c | ramps n | or heat rolong | exhaus ed expo | stion lil osure a | kely, an nd/or n | d heat⊭ hvsical | stroke j activity | oossibl / | e with | | |
| | | Extr Dar | eme Iger | 12 hi | 5°F or gher | | | 5.0.19 | Heat | stroke | highly | likely | Lourn | | | | |

(Source: US National Weather Service)





Court Ruling of Judge Calhoun

- "no evidence was presented to establish the scientific basis for the risk categories depicted on the NWS heat index chart."
- In Addition, OSHA had failed to provide any
- "....supporting data ... for why the levels of risk [indicated by the chart's color coding and legend] are attributed to their respective temperatures."



Three tired approach

- 1. A basic heat stress risk assessment questionnaire or a simple index
- 2. If a potential problem is indicated from the initial step, then the progression to a second level rational index.
- 3. Where the allowable exposure time is less than 30 minutes or there is a high involvement level of personal protective equipment (PPE), then some form of physiological monitoring should be employed.



The Challenge

Early 2021

- Mining/exploration company in the WA East Pilbara region was looking for a similar model.
 - Easy to use in the field
 - Suitable for non-technical personnel
 - Require minimal technical equipment
 - Based on substantive physiological model

Most important.

It had to be simple!



Step 1 - Develop a reference table based on a valid physiological base.

International standard - ISO 7933 Predicted Heat Strain

Required inputs:

- Dry bulb temperature (°C)
 Air Velocity m/s
 Relative humidity (%)
 Globe Temperature (°C)
 Clothing insulation factor (clo)
 Metabolic workrate (w/m²)
 Site Weather Station
 Calculated from Solar Radiation (w/m²)
 Standard Cotton Drill - ISO 9920
 Clothing insulation factor (clo)
 Physical demand assessment – ISO 8996
 Metabolic workrate (w/m²)
 Sitting, Standing, Crouched
- 8. Acclimatisation



Environmental Data Calculations

- Four variable data sets
- Every day for two months December & January
- 12 hours of data each day 0600 -1800hrs
- Averaged over 15 minutes
- 48 samples X 62 Days X 24 variable configurations
- = Lots & lots of data sets



Three key decisions were made at this point

a) Data would be averaged hourly instead of 15 minutes for three key periods of the work shift, morning, midday and afternoon.

b)Three tables would be developed rather than one, based on set metabolic loads.

- I. High workload (230 W/m²)
- II. Medium workload (175 W/m²)
- III.Low Workload (115 W/m²)
- c) Instead of using all the varying air velocities, one based on the average air velocity.



The Table Build

| | | | High | High | Mod | Mod | Low | Low | | | | | | | | | | | | | | | | | | | | | | | | | |
|----|----|----------------|--------|--------|--------|--------|--------|--------|--------|------|------|-------|------|-------|----------------|-----------|-----------------------|---------|-------|---------|----------|--------|-------------|------|-----|------|----------|---------|--------|---------|---------|-------|--------|
| | | | 4.4m/s | 4.4m/s | 4.4m/s | 4.4m/s | 4.4m/s | 4.4m/s | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | Core T | Fluid | Core T | Fluid | Core T | Fluid | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | 38 | Loss | 38 | Loss | 38 | Loss | | | | | | | | | | | | | | | | | | | | | | | | | |
| Ta | GT | RH% | (min) | (mls) | (min) | (mls) | (min) | (mls) | | | | | | | | | | | | | | | | | | | | | | | | | |
| 30 | 36 | 61.1 | | | | | | | | | | HIGH | WOR | KLOA | 1D (2 3 | 30 ¥h | m2) (T | ime to | 38. | C) 4.4 | mis | | | | HIG | HWO | RKLO | DAD (2 | 30 Wh | m2) (Ti | me to 3 | 8°C)4 | .4 m/s |
| 31 | 36 | 61.5 | | | | | | | | | | | | Rel | ative | Humie | dity % | | | | | | | | | | R | elative | e Humi | dity % | | | |
| 31 | 38 | 61.4 | | | | | | | Temp (| 10 1 | 5 20 | 25 3 | 0 35 | 5 40 | 45 | 50 5 | 5 60 | 65 7 | 70 | 75 | 80 | Temp 1 | 10 1 | 5 20 | 25 | 30 3 | 35 4 | 0 45 | 50 5 | 5 60 | 65 70 |) 75 | 80 |
| 32 | 38 | 59.2 | 54 | 7169 | NE | 5586 | NE | 3981 | 32 | | | | | | | | | | | | | 32 | | | | | | | | | | | |
| 32 | 39 | 63.9 | 61 | 7634 | NE | 5962 | NE | 4292 | 33 | | | | | | | | | | | | | 33 | | | | | | | | | | | |
| 32 | 39 | 56.2 | 47 | 7392 | NE | 5824 | NE | 4214 | 34 | | | | | | | | _ | | | | | 34 | | | | | | | | | | | |
| 32 | 40 | 55.4 | 43 | 7745 | NE | 6148 | NE | 4505 | 35 | | | | | | | | _ | | | | | 35 | | | | | | | | | | | |
| 32 | 37 | 55.6 | 53 | 6791 | NE | 5265 | NE | 3708 | 36 | | | | | | | | | | | | | 36 | | | | | | | | | _ | | |
| 33 | 39 | 63.6 | 60 | 7835 | NE | 6111 | NE | 4406 | 37 | | | | | | | | | | | | | 37 | | | | | | | | | | | |
| 33 | 37 | 59.5 | 60 | 6925 | NE | 5301 | NE | 3692 | 38 | | | | | | | | | | | | | 38 | | | | | | | | | | | |
| 33 | 35 | 55.9 | 57 | 6342 | NE | 4796 | NE | 3255 | 39 | | | | | | | | | | | | | 39 | | | | | | | | | | | |
| 33 | 37 | 53.1 | 47 | 6934 | NE | 5377 | NE | 3797 | 40 | | | | | _ | | | | | | | | 40 | | | | | | | | | | | |
| 33 | 43 | 43 | 33 | 8377 | NE | 6827 | NE | 5174 | 41 | | | | | | | | | | | | | 41 | | | | | | | | | | | |
| 34 | 42 | 57 | 42 | 8677 | NE | 6906 | NE | 5138 | 42 | | | | | | | | | | | | | 42 | | | | _ | | | | | | | |
| 34 | 38 | 51 | 42 | 7180 | NE | 5592 | NE | 3983 | 43 | | | _ | | | | | | | | | | 43 | | | _ | | | | | | | | |
| 34 | 38 | 50.8 | 42 | 7174 | NE | 5589 | NE | 3982 | 44 | | _ | | | | | | | | | | | 44 | | _ | | | | | | | | | |
| 34 | 43 | 53.4 | 37 | 8820 | NE | 7099 | NE | 5347 | 45 | | | | | | | | | | | | | 45 | | | | | | | | | | | |
| 34 | 44 | 36 | 30 | 8592 | NE | 7057 | NE | 5398 | 46 | | | | | | | | 63 | | | | | 46 | | | | | | | | | | | |
| 34 | 42 | 47.4 | 35 | 8269 | NE | 6657 | NE | 4980 | 47 | | | | _ | | | | | | | | | 47 | | | | | | | | | | | |
| 34 | 36 | 41 | 40 | 6413 | NE | 4958 | NE | 3453 | | | | MODE | RATE | E WOF | RKLO | DAD (1 | 75 WI | m2) (Ti | ime I | to 38' | C) 4.4 m | ils | | | | | | | | | | | |
| 35 | 43 | 46 | 31 | 8350 | NE | 6806 | NE | 5155 | - | | | | | Rel | ative | Humie | dity % | | | | | | | | | | | | | | | | |
| 35 | 44 | 52.0 | 36 | 9270 | NE | 7481 | NE | 5678 | Temp 1 | 10 1 | 5 20 | 25 3 | 0 35 | 5 40 | 45 | 50 5 | 5 60 | 65 | 10 | 75 | 80 | | | | | | | | | | | | |
| 35 | 40 | 48.7 | 38 | 7831 | NE | 6183 | NE | 4511 | 32 | | | | | _ | | _ | | | _ | | • | The | red | 70 | ne | 25 2 | are | י> ב | 30 i | mir | nute | ۵S | |
| 35 | 45 | 35 | 29 | 8930 | NE | 7362 | NE | 5671 | 33 | | | | | | | | | | | | | inc | | | | | | | | | | | |
| 35 | 41 | 54.3 | 40 | 8475 | NE | 6706 | NE | 4948 | 34 | | | | _ | | | | _ | | | | | | | | | | | | | | | | |
| 35 | 43 | 52 | 37 | 8936 | NE | 7169 | NE | 5390 | 35 | | | | _ | | | | | | | | | The | <u> - m</u> | ha | r 7 | 00 | . | Short | | 170 | m | inu | toc |
| 35 | 40 | 46.4 | 36 | 7746 | NE | 6134 | NE | 4483 | 36 | | | | | | | | | | | | • | me | am | ne | 1 2 | OH | 1e - | 25U | ノン | | חוי | mu | les |
| 35 | 40 | 51.6 | 40 | 7956 | NE | 6256 | NE | 4554 | 37 | | | | _ | | | | | | | | | | | | | | | | | | | | |
| 35 | 38 | 48 | 39 | 7214 | NE | 5612 | NE | 3994 | 38 | _ | | | | _ | | | | | | | | | | | - | | | | | | | | |
| 35 | 41 | 48.1 | 36 | 8108 | NE | 6454 | NE | 4765 | 39 | | | | | | | | | | | | • | The | vel | lov | v t | ror | m : | >12 | 2() < | < 74 | 10 | | |
| 35 | 41 | 43. r 40. 1 | 35 | 7358 | NE | 0305 | NE | 4(1) | 40 | | | | | - | | | | | | | | | , | | | ••• | | | | | | | |
| 35 | 40 | 49.1 | 38 | 10200 | NE | 0132 | NE | 4516 | 41 | _ | | | - | | | | | | | | | | .+~ | ~ | | | | | | | | | |
| 35 | 49 | 41.8 | 28 | 10338 | NE | 8018 | NE | 6858 | 42 | | _ | - | | | | | | | | | | mini | lle | 5. | | | | | | | | | |
| 30 | 44 | 41.8 | 31 | 8920 | NE | 7256 | NE | 5523 | 43 | | | | | | | | | | | | | | | | | | | | | | | | |
| 30 | 44 | 41 | 23 | 8592 | NE | 7052 | NE | 5389 | 44 | | _ | | | | | | | | | | | | | | | | | | | | | | |
| 30 | 45 | 42.0 | 31 | 3253 | TE | 1565 | NE | 3806 | 45 | | | | | | | | | | | | | | | | | | | | | | | | |
| 30 | 51 | 43.9 | 20 | 11412 | 75 | 3358 | NE | 1062 | 46 | | | | | | | | | | | | | | | | | | | | | | | | |
| 30 | 42 | 45.0 | 34 | 0432 | NE | 0752 | NE | 5035 | 47 | | | 1000 | JOP | | D (14 | - L J L - | э) (Т • | | 0.0 | 744 | - 1- | | | | | | | | | | | | |
| 30 | 40 | 42.0 | 23 | 3372 | NE | 1131 | NE | 3335 | | | | LOA / | TORF | | D (II) | 5 ¥/m | 2) () in 1999 () | ne to 3 | σL | , 1 4.4 | mrs | | | | | | | | | | | | |
| 30 | 42 | 4Z.Z | 33 | 0320 | NE | 0004 | NC | 4332 | | | | | | Hel | ative | riumie | aity % | | | | | | | | | | | | | | | | |



PHS Tables

| | | | | _ | MEDIUM WORKLOAD (175 W/m2) | | | | | | | | | | | | | | | | | | |
|---------|----|----|----|---|----------------------------|----|----|----|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| | | | | | | | | | HIGH WORKLOAD (230 W/m2) (Time to 38°C) | | | | | | | | | | | | | | |
| Temp °C | 10 | 15 | 20 | 2 | Temp °C | 10 | 15 | 20 | Relative Humidity % | | | | | | | | | | | | | | |
| 32 | | | | | 32 | | | | Temp °C | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 |
| 33 | | | | | 33 | | | | 32 | | | | | | | | | | | | | | |
| 34 | | | | | 34 | | | | 33 | | | | | | | | | | | | | | |
| 35 | | | | | 35 | | | | 34 | | | | | | | | | | | | | | |
| 36 | | | | | 36 | | | | 35 | | | | | | | | | | | | | | |
| 37 | | | | | 37 | | | | 36 | | | | | | | | | | | | | | |
| 38 | | | | | 38 | | | | 37 | | | | | | | | | | | | | | |
| 39 | | | | | 39 | | | | 38 | | | | | | | | | | | | | | |
| 40 | | | | | 40 | | | | 39 | | | | | | | | | | | | | | |
| 41 | | | | | 41 | | | | 40 | | | | | | | | | | | | | | |
| 42 | | | | | 42 | | | | 41 | | | | | | | | | | | | | | |
| 43 | | | | | 43 | | | | 42 | | | | | | | | | | | | | | |
| 44 | | | | | 44 | | | | 43 | | | | | | | | | | | | | | |
| 45 | | | | | 45 | | | | 44 | | | | | | | | | | | | | | |
| 46 | | | | | 46 | | | | 45 | | | | | | | | | | | | | | |
| 47 | | | | | 47 | | | | 40 | | | | | | | | | | | | | | |

Trigger Action Response Guide





Simplified Heat Stress Chart System

- Similar to the National Weather Service HSI Charts but is based on ISO 7933 for physiological risk.
- Only requires knowledge of:
 - Air temperature,
 - Humidity, and
 - estimated workload.



Results from first year use in the field

- Feedback indicated that process met simplicity criteria
- Suitable for the first level assessment for planning
- Overall reduction in heat related incidence from **forty** in previous year to **four**.
- Still some further development & validation required in different environments



Limitations

- Heat stress index calculations are based on fit, healthy participants, 90kg, 1.8m.
- 2. Globe temperatures were calculated from meteorological data.
- 3. An averaged air velocity for the period was used rather than multiple variables.
- 4. Data from two months of the year: a larger database would have been preferred.
- 5. Posture was limited to standing.
- 6. ISO 7933 has not been fully validated for some of the extreme conditions experienced.



Important Caveats





